

FORUM WOOD BUILDING NORDIC

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PREMIUM PARTNERS



Hygro-thermal modeling of timber bridge decks considering the effect of solar radiation

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Click Design (ForestValue)

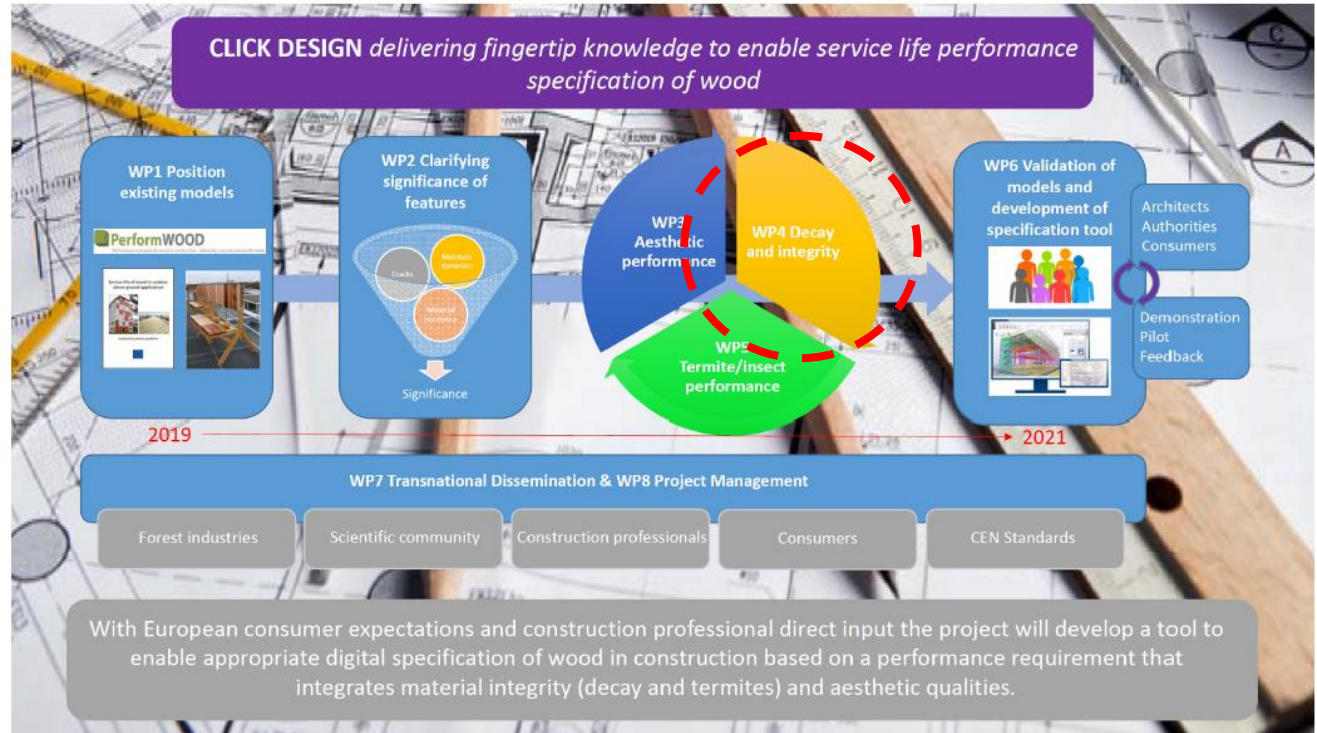
Coordinator: BRE (UK), 28 partners; **Scientific partners:** Goettingen University (DE), Lund University (SE), VTT Ltd (FI), InnoRenew CoE (SI), FCBA (FR), NIBIO (NO) - Duration: March 2019-June 2022

Finnish funder: Ympäristöministeriö

Finnish partners

- VTT (WP4 leader)
- Väylävirasto
- Puutuoteteollisuus
- Stora Enso

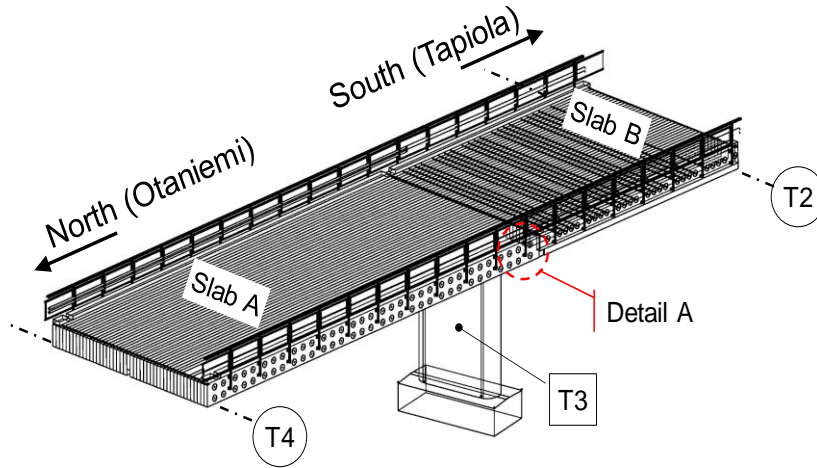
ForestValue



Monitoring of Tapiola Bridge in Espoo

Tapiola Bridge

Transverse prestressed glulam wooden slabs



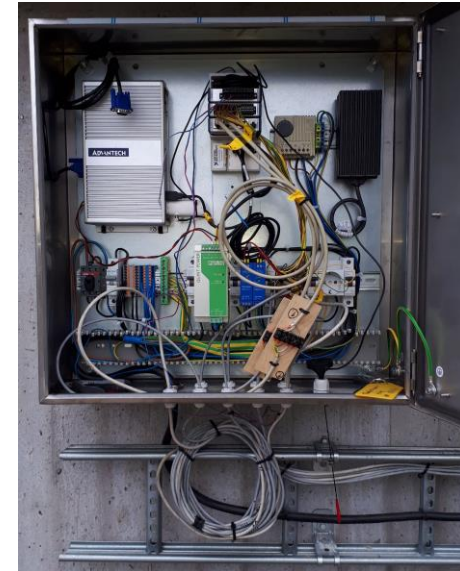
- 46 timber beams in the width direction
- beam widths = 0.215 m, heights = 0.765 m for the 13.45 m span and 1.035 m for the 22.13 m span
- deck width = 9.89 m, near to useful width 9.79 m
- weak paint

Sensor-based monitoring

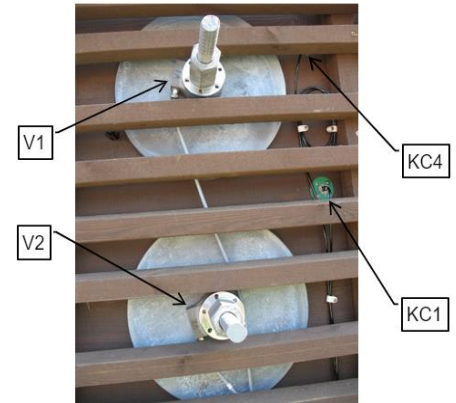
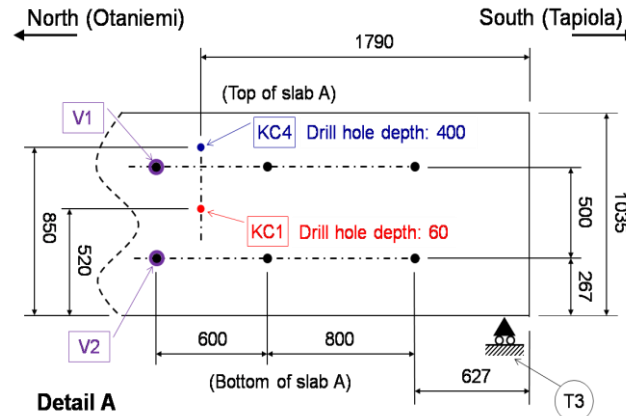
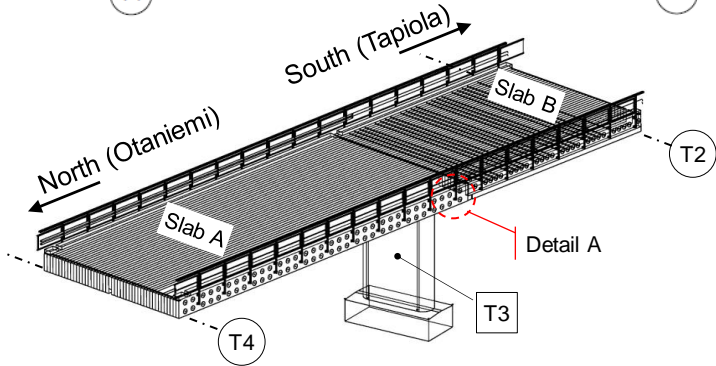
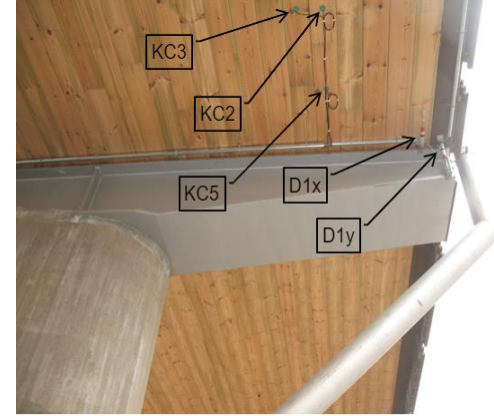
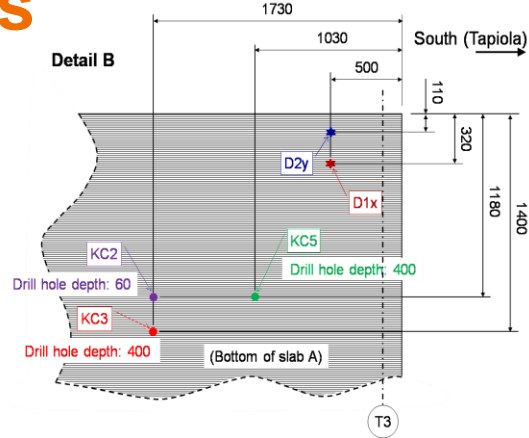
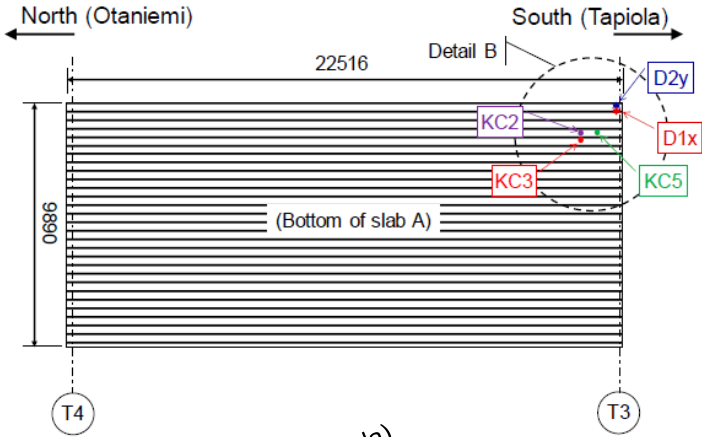
No.	ID	Sensor Type	Model
1	KC1	Humidity and temperature	HMP110
2	KC2	Humidity and temperature	HMP110
3	KC3	Humidity and temperature	HMP110
4	KC4	Humidity and temperature	HMP110
5	KC5	Humidity and temperature	HMP110
6	V1	Force	C6A
7	V2	Force	C6A
8	D1x	Slab longitudinal displacement	ELPC100 linear potentiometer of OPKON
9	D2y	Slab vertical displacement	ELPC 100 linear potentiometer of OPKON



Monitoring station with on-board computer



Locations of sensors



Multi-phase model for simulation of moisture transport in wood below the FSP

Multi-phase model – Governing equations

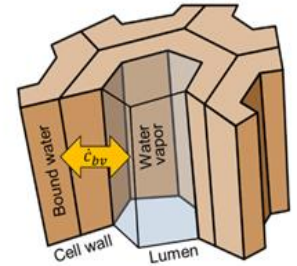
Phenomena below the fibre saturation point (FSP) of wood modeled through coupled differential equations and implemented in Uel subroutine of Abaqus FEM code

- Diffusion of bound water in wood cell walls
- Diffusion of vapour water in lumens
- Conservation energy (thermal equation)

$$\frac{\partial c_b}{\partial t} = -\nabla \cdot \mathbf{J}_b + \dot{c}_{bv}$$

$$\frac{\partial c_v}{\partial t} = -\nabla \cdot \mathbf{J}_v - \dot{c}_{bv}$$

$$c_w \rho \frac{\partial T}{\partial t} = -\nabla \cdot \mathbf{J}_H - \nabla \cdot \mathbf{J}_b h_b - \nabla \cdot \mathbf{J}_v h_v + \dot{c}_{bv} h_{bv}$$



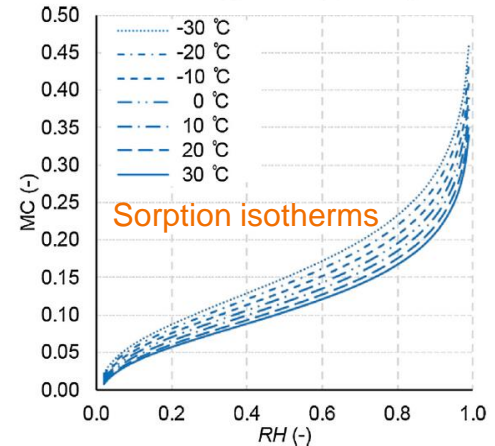
with fluxes $\mathbf{J}_b = -D_b \nabla c_b$, $\mathbf{J}_v = -D_v \nabla c_v$, $\mathbf{J}_H = -K \nabla T$

- Sorption between water phases



Results: moisture content (MC), temperature (T) and relative humidity (RH) in wood

Fortino S., Hradil P., Genoese A., Genoese A., Pousette, A. Numerical hygro-thermal analysis of coated wooden bridge members exposed to Northern European climates. Construction and Building Materials 208, 492–505 (2019)



Boundary conditions

Boundary conditions for variables concentration of bound water and water vapour

$$\mathbf{n} \cdot \mathbf{J}_b = 0, \quad \mathbf{n} \cdot \mathbf{J}_v = k_v^w c_v^l - k_v^a c_v^a,$$

Boundary conditions for temperature including the net variance at the wood surface

$$\mathbf{n} \cdot \mathbf{J}_v = k_T (T - T^a) - q$$

Net variance at the wood surface, function of Cos (I)

$$q = \alpha G + \varepsilon L - \varepsilon \sigma T_s^4$$

α : solar absorptivity

G : incident solar radiance

L : incident long-wave radiation

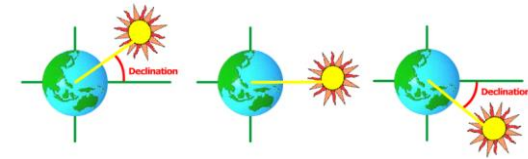
ε : long-wave emissivity

σ : Stefan-Boltzmann constant

T_s : surface temperature

Declination angle

$$\delta = -23.45^\circ \times \cos\left(\frac{360}{365} \times (d + 10)\right)$$



$$\cos(I) = \cos(h)\cos(A_{ss})\sin(E) + \sin(h)\cos(E)$$

I: incident angle on a surface

h: solar altitude, function of declination angle

Ass: surface-solar azimuth

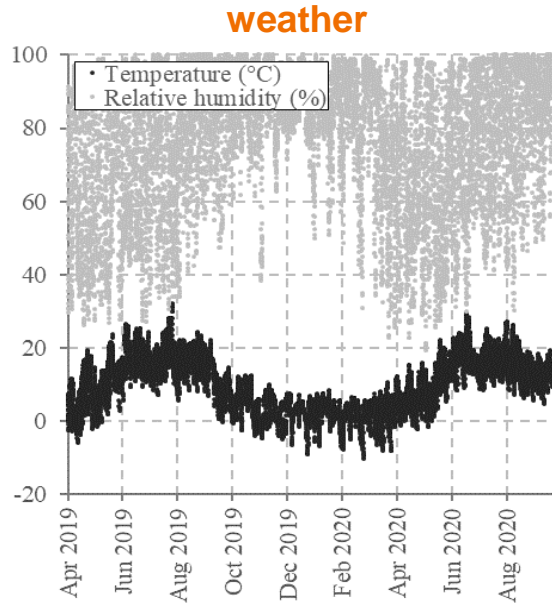
E: the angle of the surface from horizontal

Kang W., Lee Y-H., Kang C-W., Chung W-Y., Xu H-L., Matsamura J. Using the Inverse Method to Estimate the Solar Absorptivity and Emissivity of Wood Exposed to the Outdoor Environment. J. Fac. Agr., Kyushu Univ., 56 (1), 139–148 (2011)

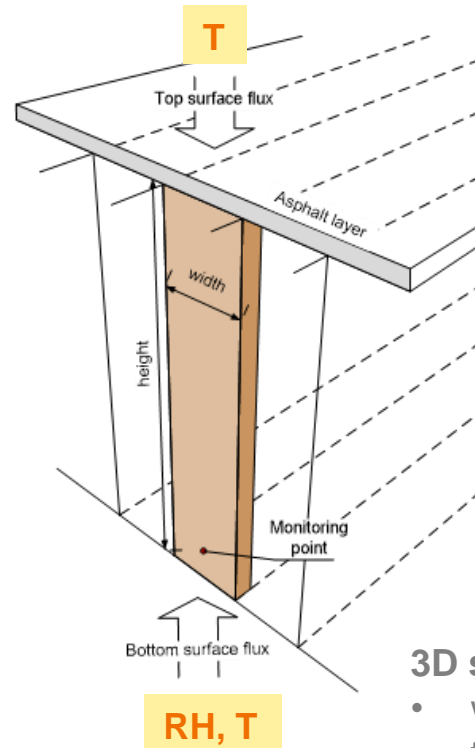
C.J.J. Castenmiller Surface temperature of wooden window frames under influence of solar radiation. TNO Building and Construction, Delft, The Netherlands. HERON, Vol. 49, No. 4 (2004)

Hygro-thermal analysis of Tapiola Bridge's deck

Model in Abaqus FEM code



- Initial relative humidity $RH_0 = 65\%$
- Initial temperatures $T_0 = 0.85\text{ °C}$
- initial moisture content in equilibrium with RH_0
→ $MC_0 = 15.3\%$



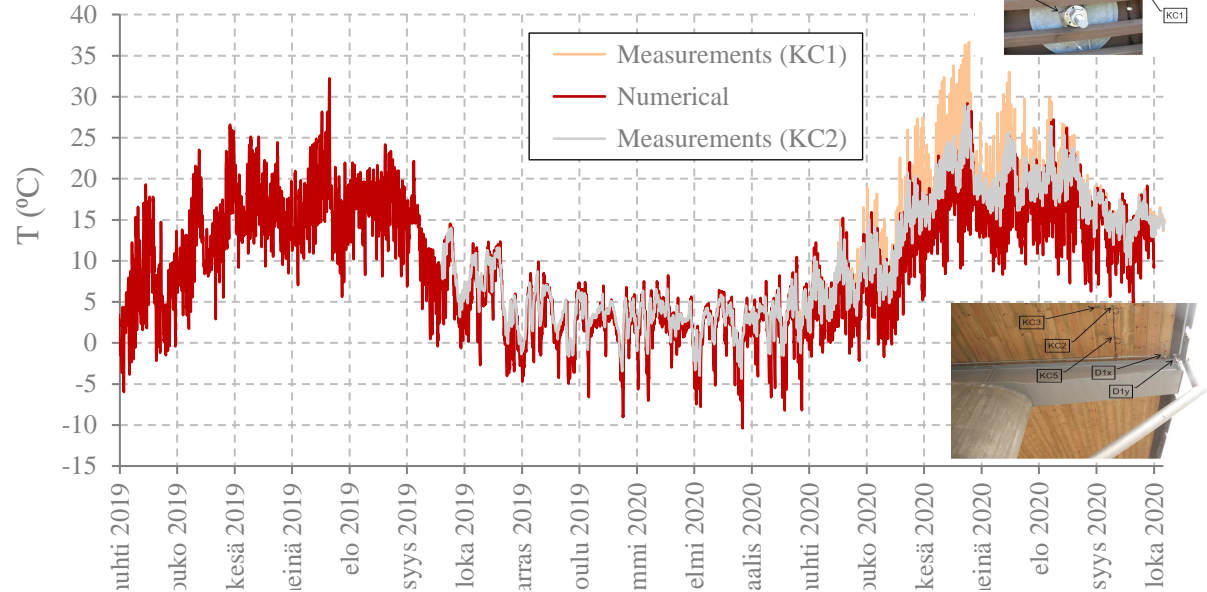
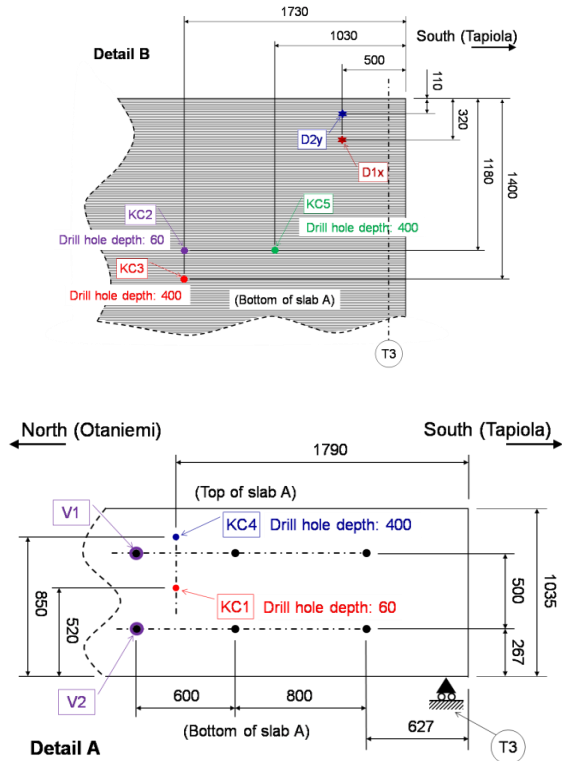
boundary conditions

**RH, T,
solar radiation**

3D slice

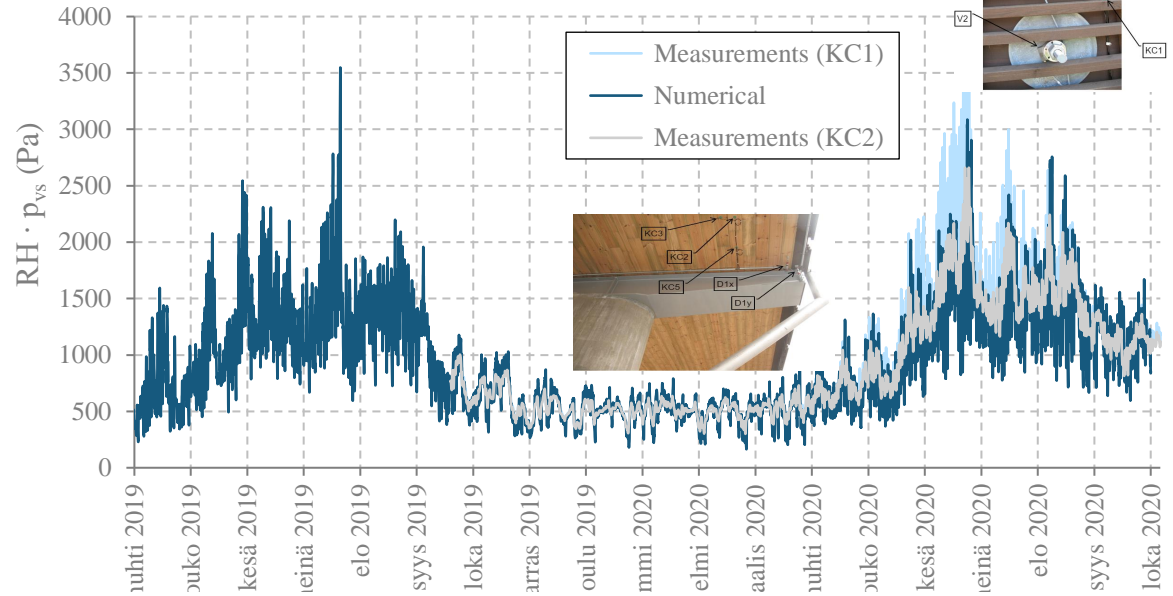
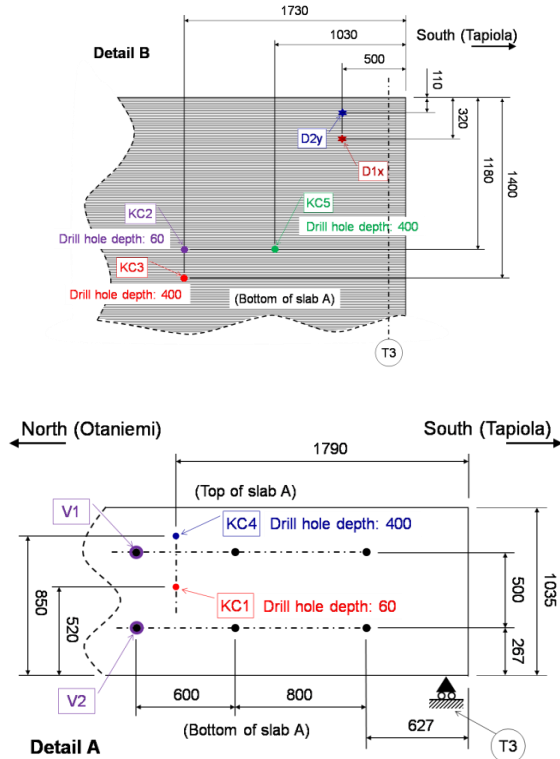
- width = 107.5 mm (half of the lamination)
- height 1035 mm
- thickness 5 mm

Numerical results – Temperature



- **Measurements at 60 mm from surface:** slightly higher temperature peaks in KC1 in summer time from the lateral side exposed to the afternoon sun
- **Numerical model:** the current model shows an increase of temperature peaks below 5% compared to the model without the solar radiation effect

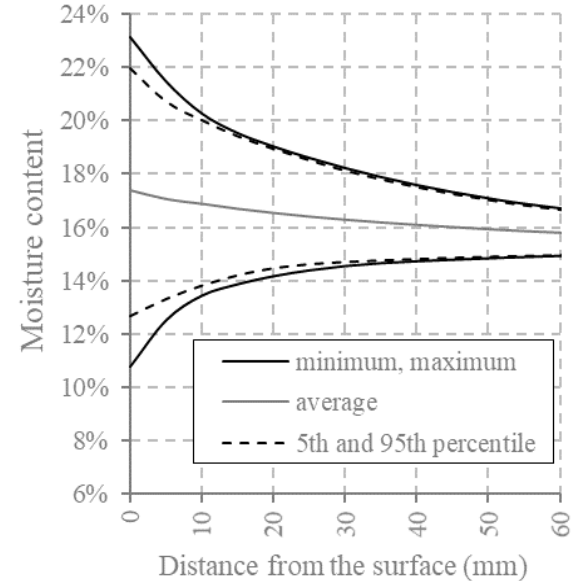
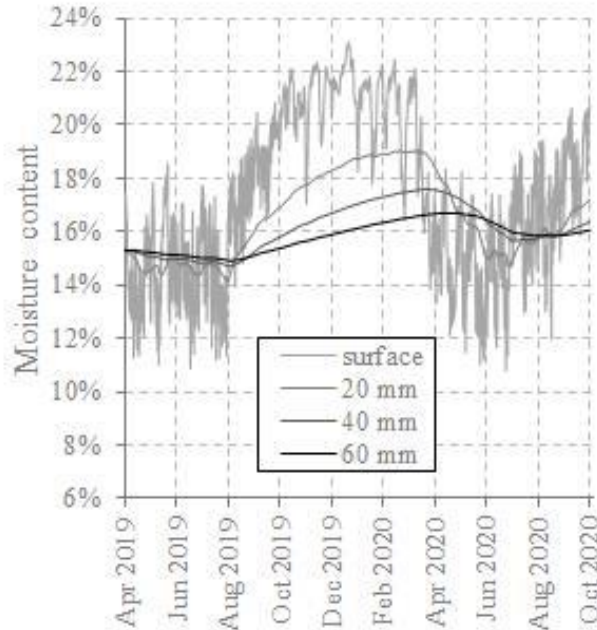
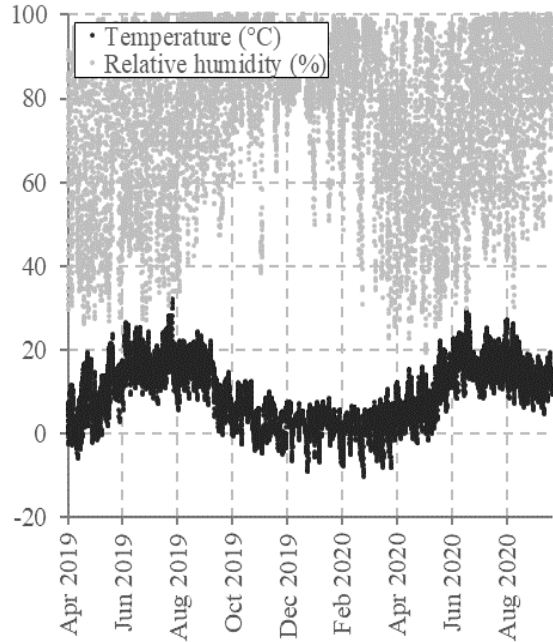
Numerical results – Relative humidity



Saturated vapour pressure

$$p_{vs} = \begin{cases} \exp\left(53.421 - \frac{6516.3}{T} - 4.125 \ln(T)\right) & \text{for } T \geq 0^\circ\text{C} \\ 100 \times 10^{\frac{9.5(T-273.15)}{T-7.65} + 0.7858} & \text{for } T < 0^\circ\text{C} \end{cases}$$

Numerical results – Moisture content



Discussion and future work

- Smart monitoring with implemented early warning systems can substantially decrease maintenance costs of timber bridges
- The current multi-phase model including solar radiation effects provides a small increase of temperature peaks in summer time (below 5%). The effect is negligible for the MC in wood
- Moisture peaks remain below 23% because Tapiola Bridge is protected, even if the used paint has low vapour resistance
- The average values of MC should not change significantly during the successive years
- The average MCs are around 16% up to 20 mm depth, and remain at an almost constant level up until 60 mm depth. However, 50% of the pre-loading force loss was measured before retightening in June 2022. Cupping phenomena should be investigated.
- The displacements and forces measured in the other sensors can be simulated in future work by integrating the hygro-thermal analysis with a mechanical model for wood
- The monitoring is currently on-going. The work will continue within the EU 5G-TIMBER project

New projects

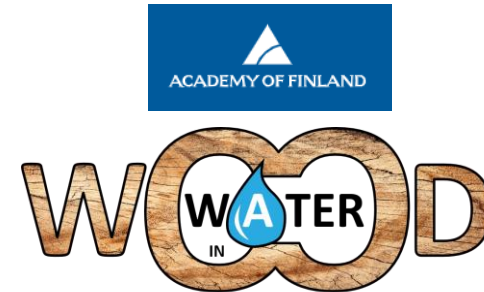
Secure 5G-Enabled Twin Transition for Europe's TIMBER Industry Sector (5G-TIMBER)

- **HEU call:** CL4-2021-TWIN-TRANSITION-01-08: Data-driven Distributed Industrial Environments (IA)
- **Coordinator:** Tallinn University of Technology, 16 partners; **Duration:** 1.6.2022-31.5.2025
- **Main VTT's topics:** digital wood material models, IoT for predictive maintenance and structural health monitoring

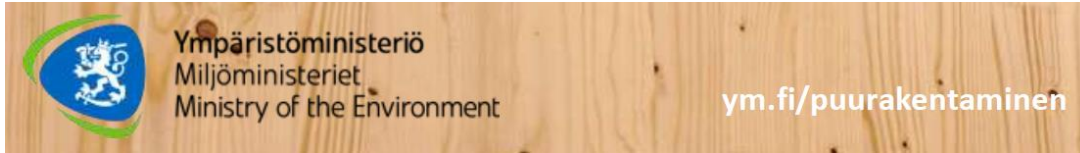


Image-based Modelling of Water Transport In Wood including material biodegradation (WaterInWood)

- **Coordinator:** VTT Technical Research Centre of Finland
- **Partners:** University of Jyväskylä, LUKE - Natural Resources Institute Finland; **Duration:** 1.9.2021-31.08.2025
- **Main aim:** to fundamentally improve understanding on water transport in wood in hygroscopic and over-hygroscopic conditions and in the initial phases of fungal decay



WaterInWood project • 2022 - 2025 • Academy of Finland



Thank you!
Questions?



Puutuoteteollisuus

JARTEK

